## 64-Position OTP Digital Potentiometer

## FEATURES

## 64 positions

One-time programmable (OTP) ${ }^{1}$ set-and-forget
Resistance setting-low cost alternative over EEMEM
Unlimited adjustments prior to OTP activation
$1 \mathrm{k} \Omega, 10 \mathrm{k} \Omega, 50 \mathrm{k} \Omega, 100 \mathrm{k} \Omega$ end-to-end terminal resistance
Compact 8-lead SOT-23 standard package
Ultralow power: $\mathrm{IDD}_{\mathrm{D}}=5 \mu \mathrm{~A}$ maximum
Fast settling time: $\mathrm{t}_{\mathrm{s}}=5 \boldsymbol{5}$ s typical during power-up
$I^{2} \mathrm{C}$-compatible digital interface
Computer software ${ }^{2}$ replaces microcontroller in factory programming applications
Wide temperature range: $-\mathbf{4 0}{ }^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$
Low operating voltage: 2.7 V to 5.5 V
OTP validation check function

## APPLICATIONS

## System calibrations

Electronics level settings
Mechanical potentiometers and trimmer replacement
Automotive electronics adjustments

## Transducer circuit adjustments

Programmable filters up to $6 \mathbf{M H z} \mathrm{BW}^{3}$

## GENERAL DESCRIPTION

The AD5273 is a 64-position, one-time programmable (OTP) digital potentiometer ${ }^{4}$ that employs fuse link technology to achieve permanent program setting. This device performs the same electronic adjustment function as most mechanical trimmers and variable resistors. It allows unlimited adjustments before permanently setting the resistance values. The AD5273 is programmed using a 2 -wire, $\mathrm{I}^{2} \mathrm{C}^{\ominus}$-compatible digital control. During write mode, a fuse blow command is executed after the final value is determined, thereby freezing the wiper position at a given setting (analogous to placing epoxy on a mechanical trimmer). When the permanent setting is achieved, the value does not change, regardless of the supply variations or environmental stresses under normal operating conditions. To verify the success of permanent programming, Analog Devices, Inc., patterned the OTP validation such that the fuse status can be discerned from two validation bits in the read mode.


Figure 1.
In addition, for applications that program the AD5273 at the factory, Analog Devices offers device programming software ${ }^{2}$ running on Windows ${ }^{\star} \mathrm{NT}^{\star}$, Windows 2000, and Windows XP operating systems. This software application effectively replaces any external $\mathrm{I}^{2} \mathrm{C}$ controllers, which in turn enhances the user system's time-to-market.
The AD5273 is available in $1 \mathrm{k} \Omega, 10 \mathrm{k} \Omega, 50 \mathrm{k} \Omega$, and $100 \mathrm{k} \Omega$ resistances and in a compact 8 -lead SOT-23 standard package. It operates from $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$.

Along with its unique OTP feature, the AD5273 lends itself well to general digital potentiometer applications due to its effective resolution, array resistance options, small footprint, and low cost.

An AD5273 evaluation kit and software are available. The kit includes the connector and cable that can be converted for factory programming applications.

For applications that require dynamic adjustment of resistance settings with nonvolatile EEMEM, users should refer to the AD523x and AD525x families of nonvolatile memory digital potentiometers.

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## AD5273

## SPECIFICATIONS

$\mathrm{V}_{\mathrm{DD}}=2.7 \mathrm{~V}$ to $5.5 \mathrm{~V}, \mathrm{~V}_{\mathrm{A}}<\mathrm{V}_{\mathrm{DD}}, \mathrm{V}_{\mathrm{B}}=0 \mathrm{~V},-40^{\circ} \mathrm{C}<\mathrm{T}_{\mathrm{A}}<+105^{\circ} \mathrm{C}$, unless otherwise noted.
Table 1.

| Parameter | Symbol | Conditions | Min | Typ ${ }^{1}$ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| DC CHARACTERISTICS—RHEOSTAT MODE Resolution | N |  |  |  | 6 | Bits |
| Resistor Differential Nonlinearity ${ }^{2}$ | R-DNL |  |  |  |  |  |
| $10 \mathrm{k} \Omega, 50 \mathrm{k} \Omega, 100 \mathrm{k} \Omega$ |  | $\mathrm{R}_{\mathrm{WB}}, \mathrm{V}_{\mathrm{A}}=\mathrm{NC}$ | -0.5 | +0.05 | $+0.5$ | LSB |
| $1 \mathrm{k} \Omega$ |  | $\mathrm{RwB}_{\text {w }}, \mathrm{V}_{\mathrm{A}}=\mathrm{NC}$ | -1 | +0.25 | +1 | LSB |
| Resistor Nonlinearity ${ }^{2}$ | R-INL |  |  |  |  | LSB |
| $10 \mathrm{k} \Omega, 50 \mathrm{k} \Omega, 100 \mathrm{k} \Omega$ |  | Rwi, $\mathrm{V}_{\mathrm{A}}=\mathrm{NC}$ | -0.5 | +0.10 | +0.5 | LSB |
| $1 \mathrm{k} \Omega$ |  | $\mathrm{R}_{\mathrm{WB}}, \mathrm{V}_{\mathrm{A}}=\mathrm{NC}$ | -5 | +2 | +5 | LSB |
| Nominal Resistance Tolerance ${ }^{3}$ $10 \mathrm{k} \Omega, 50 \mathrm{k} \Omega, 100 \mathrm{k} \Omega$ | $\Delta \mathrm{R}_{A B} / \mathrm{R}_{\text {AB }}$ | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | -30 |  | +30 | \% |
| Nominal Resistance, $1 \mathrm{k} \Omega$ | $\mathrm{R}_{\text {AB }}$ |  | 0.8 | 1.2 | 1.6 | $\mathrm{k} \Omega$ |
| Rheostat Mode Temperature Coefficient ${ }^{4}$ | $\left(\Delta R_{A B} / R_{A B}\right) / \Delta T$ | Wiper $=$ NC |  | 300 |  | ppm/ ${ }^{\circ} \mathrm{C}$ |
| Wiper Resistance | Rw | $\mathrm{I}_{\mathrm{w}}=\mathrm{V}_{\mathrm{DD}} / \mathrm{R}, \mathrm{V} \mathrm{DD}=3 \mathrm{~V}$ or 5 V |  | 60 | 100 | $\Omega$ |
| DC CHARACTERISTICS—POTENTIOMETER DIVIDER MODE |  |  |  |  |  |  |
| Differential Nonlinearity ${ }^{5}$ | DNL |  | -0.5 | +0.1 | +0.5 | LSB |
| Integral Nonlinearity ${ }^{5}$ | INL |  | -0.5 |  | +0.5 | LSB |
| Voltage Divider ${ }^{4}$ Temperature Coefficient | $\left(\Delta \mathrm{V}_{\mathrm{w}} / \mathrm{V}_{\mathrm{w}}\right) / \Delta \mathrm{T}$ | Code $=0 \times 20$ |  | 10 |  | ppm/ ${ }^{\circ} \mathrm{C}$ |
| Full-Scale Error | $V_{\text {wfSE }}$ | Code $=0 \times 3 \mathrm{~F}$ | -1 |  | 0 | LSB |
| $10 \mathrm{k} \Omega, 50 \mathrm{k} \Omega, 100 \mathrm{k} \Omega$ |  |  | -1 |  | 0 | LSB |
| $1 \mathrm{k} \Omega$ |  |  | -6 |  | 0 | LSB |
| Zero-Scale Error | $\mathrm{V}_{\text {WZSE }}$ | Code $=0 \times 00$ | -6 |  | 0 | LSB |
| $10 \mathrm{k} \Omega, 50 \mathrm{k} \Omega, 100 \mathrm{k} \Omega$ |  |  | 0 |  | 1 | LSB |
| $1 \mathrm{k} \Omega$ |  |  | 0 |  | 5 | LSB |
| RESISTOR TERMINALS |  |  |  |  |  |  |
| Voltage Range ${ }^{6}$ | $\mathrm{V}_{\mathrm{A}}, \mathrm{V}_{\mathrm{B}}, \mathrm{V}_{\mathrm{W}}$ |  | GND |  | $V_{D D}$ | V |
| Capacitance ${ }^{7}$ A, B | $C_{A}, C_{B}$ | $\begin{aligned} & \mathrm{f}=5 \mathrm{MHz} \text {, measured to GND, code }= \\ & 0 \times 20 \end{aligned}$ |  | 25 |  | pF |
| Capacitance ${ }^{\text { }}$ W | $C_{w}$ | $\mathrm{f}=1 \mathrm{MHz}$, measured to GND, code $=$ $0 \times 20$ |  | 55 |  | pF |
| Common-Mode Leakage | I cm | $\mathrm{V}_{\mathrm{A}}=\mathrm{V}_{\mathrm{B}}=\mathrm{V}_{\mathrm{W}}$ |  | 1 |  | nA |
| DIGITAL INPUTS AND OUTPUTS |  |  |  |  |  |  |
| Input Logic High (SDA and SCL) ${ }^{8}$ | $\mathrm{V}_{\text {IH }}$ |  | $\begin{array}{l\|l} 0.7 \\ V_{D D} \end{array}$ |  | $\begin{aligned} & V_{D D}+ \\ & 0.5 \end{aligned}$ | V |
| Input Logic Low (SDA and SCL) ${ }^{8}$ | VIL |  | -0.5 |  | $\begin{aligned} & +0.3 \\ & V_{D D} \end{aligned}$ | V |
| Input Logic High (ADO) | $\mathrm{V}_{\text {IH }}$ |  | 3.0 |  | V ${ }_{\text {D }}$ | V |
| Input Logic Low (ADO) | $\mathrm{V}_{\text {IL }}$ | $\mathrm{V}_{\mathrm{IN}}=0 \mathrm{~V}$ or 5 V | 0 |  | 0.4 | V |
| Input Logic Current | ILI |  |  | 0.01 | 1 | $\mu \mathrm{A}$ |
| Input Capacitance ${ }^{7}$ | CIL |  |  | 3 |  | pF |
| Output Logic Low (SDA) | VoL |  |  |  | 0.4 | V |
| Three-State Leakage Current | loz |  |  |  | $\pm 1$ | $\mu \mathrm{A}$ |
| Output Capacitance ${ }^{7}$ | Coz |  |  | 3 |  | pF |


| Parameter | Symbol | Conditions | Min | Typ ${ }^{1}$ | Max | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| POWER SUPPLIES |  |  |  |  |  |  |
| Power Supply Range | $V_{D D}$ |  | 2.7 |  | 5.5 | V |
| OTP Power Supply ${ }^{8,9}$ | VDD_OTP | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$ | 4.75 | 5 | 5.25 | V |
| Supply Current | IDD | $\mathrm{V}_{\mathrm{IH}}=5 \mathrm{~V}$ or $\mathrm{V}_{\mathrm{IL}}=0 \mathrm{~V}$ |  | 0.1 | 5 | $\mu \mathrm{A}$ |
| OTP Supply Current ${ }^{8,10,11}$ | IDD_OTP | $\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}, \mathrm{V}_{\text {DD_OTP }}=5 \mathrm{~V}$ |  | 100 |  | mA |
| Power Dissipation ${ }^{12}$ | Pdiss | $\mathrm{V}_{\mathrm{H}}=5 \mathrm{~V}$ or $\mathrm{V}_{\mathrm{IL}}=0 \mathrm{~V}, \mathrm{~V}_{\text {dD }}=5 \mathrm{~V}$ |  | 0.5 | 27.5 | $\mu \mathrm{W}$ |
| Power Supply Sensitivity | PSRR | $\mathrm{R}_{\text {AB }}=1 \mathrm{k} \Omega$ | -0.3 |  | +0.3 | \%/\% |
|  | PSRR | $\mathrm{R}_{\text {AB }}=10 \mathrm{k} \Omega, 50 \mathrm{k} \Omega, 100 \mathrm{k} \Omega$ | -0.05 |  | +0.05 | \%/\% |
| DYNAMIC CHARACTERISTICS7, 13, 14 |  |  |  |  |  |  |
| Bandwidth, -3 dB | BW_1 $\mathrm{k} \Omega$ | $\mathrm{R}_{\text {AB }}=1 \mathrm{k} \Omega$, code $=0 \times 20$ |  | 6000 |  | kHz |
|  | BW_10 k $\Omega$ | $\mathrm{R}_{\mathrm{AB}}=10 \mathrm{k} \Omega$, code $=0 \times 20$ |  | 600 |  | kHz |
|  | BW_50 k | $\mathrm{R}_{\mathrm{AB}}=50 \mathrm{k} \Omega$, code $=0 \times 20$ |  | 110 |  | kHz |
|  | BW_100 k $\Omega$ | $\mathrm{R}_{\text {AB }}=100 \mathrm{k} \Omega$, code $=0 \times 20$ |  | 60 |  | kHz |
| Total Harmonic Distortion | THD ${ }_{\text {w }}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{A}}=1 \mathrm{Vrms}, \mathrm{R}_{\mathrm{AB}}=1 \mathrm{k} \Omega, \mathrm{~V}_{\mathrm{B}}=0 \mathrm{~V}, \mathrm{f}=1 \\ & \mathrm{kHz} \end{aligned}$ |  | 0.05 |  | \% |
| Adjustment Settling Time | $\mathrm{t}_{51}$ | $\begin{aligned} & \mathrm{V}_{\mathrm{A}}=5 \mathrm{~V} \pm 1 \mathrm{LSB} \text { error band, } \mathrm{V}_{\mathrm{B}}=0 \mathrm{~V} \text {, } \\ & \text { measured at } \mathrm{V}_{\mathrm{W}} \end{aligned}$ |  | 5 |  | $\mu \mathrm{s}$ |
| Power-Up Settling TimeAfter Fuses Blown | ts2 | $\begin{aligned} & \mathrm{V}_{\mathrm{A}}=5 \mathrm{~V} \pm 1 \mathrm{LSB} \text { error band, } \mathrm{V}_{\mathrm{B}}=0 \mathrm{~V} \text {, } \\ & \text { measured at } \mathrm{V}_{\mathrm{W}}, \mathrm{~V}_{\mathrm{DD}}=5 \mathrm{~V} \end{aligned}$ |  | 5 |  | $\mu \mathrm{s}$ |
| Resistor Noise Voltage | en_wb | $\mathrm{R}_{\mathrm{AB}}=1 \mathrm{k} \Omega, \mathrm{f}=1 \mathrm{kHz}$, code $=0 \times 20$ |  | 3 |  | $\mathrm{nV} / \sqrt{ } \mathrm{Hz}$ |
| INTERFACE TIMING CHARACTERISTICS7, 14, 15 |  | Applies to all parts |  |  |  |  |
| SCL Clock Frequency | fscı |  |  |  | 400 | kHz |
| $\mathrm{t}_{\text {buf }}$ Bus Free Time Between Stop and Start | $\mathrm{t}_{1}$ |  | 1.3 |  |  |  |
| thd; sta Hold Time (Repeated Start) | $\mathrm{t}_{2}$ | After this period, the first clock pulse is generated | 0.6 |  |  | $\mu \mathrm{s}$ |
| tiow Low Period of SCL Clock | $\mathrm{t}_{3}$ |  | 1.3 |  |  | $\mu \mathrm{s}$ |
| $\mathrm{t}_{\text {HIGH }}$ High Period of SCL Clock | $\mathrm{t}_{4}$ |  | 0.6 |  | 50 | $\mu \mathrm{s}$ |
| tsu; sTA Setup Time for Start Condition | $\mathrm{t}_{5}$ |  | 0.6 |  |  |  |
| $t_{\text {hd; Dat }}$ Data Hold Time | $\mathrm{t}_{6}$ |  |  |  | 0.9 | $\mu \mathrm{s}$ |
| tsu; DAt Data Setup Time | $\mathrm{t}_{7}$ |  | 0.1 |  |  | $\mu \mathrm{s}$ |
| $t_{F}$ Fall Time of Both SDA and SCL Signals | $\mathrm{t}_{8}$ |  |  |  | 0.3 | $\mu \mathrm{s}$ |
| $t_{k}$ Rise Time of Both SDA and SCL Signals | $\mathrm{t}_{9}$ |  |  |  | 0.3 | $\mu \mathrm{s}$ |
| tsu; sto Setup Time for Stop Condition | $\mathrm{t}_{10}$ |  | 0.6 |  |  | $\mu \mathrm{s}$ |
| OTP Program Time | $\mathrm{t}_{11}$ |  |  | 400 |  | ms |

[^1]
## ABSOLUTE MAXIMUM RATINGS

$\mathrm{T}_{\mathrm{A}}=25^{\circ} \mathrm{C}$, unless otherwise noted.
Table 2.

| Parameter | Rating |
| :---: | :---: |
| $V_{\text {DD }}$ to GND | -0.3 V +6.5 V |
| $\mathrm{V}_{\mathrm{A}}, \mathrm{V}_{\mathrm{B}}, \mathrm{V}_{\mathrm{w}}$ to GND | GND, VDD |
| Maximum Current |  |
| $I_{\text {we, }}$ I Iwa Pulsed | $\pm 20 \mathrm{~mA}$ |
| $\mathrm{I}_{\text {wB }}$ Continuous ( $\mathrm{R}_{\text {wb }} \leq 1 \mathrm{k} \Omega$, A Open) ${ }^{1}$ | $\pm 4 \mathrm{~mA}$ |
| Iwa Continuous ( $\mathrm{Rwa} \leq 1 \mathrm{k} \Omega$, B Open) | $\pm 4 \mathrm{~mA}$ |
| Digital Input and Output Voltage to GND | $0 \mathrm{~V}, \mathrm{~V}_{\mathrm{DD}}$ |
| Operating Temperature Range | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ |
| Maximum Junction Temperature ( $\mathrm{T}_{\mathrm{J}}$ max) | $150^{\circ} \mathrm{C}$ |
| Storage Temperature | $-65^{\circ} \mathrm{C}$ to $+150^{\circ} \mathrm{C}$ |
| Reflow Soldering |  |
| Peak Temperature | $260^{\circ} \mathrm{C}$ |
| Time at Peak Temperature | 20 sec to 40 sec |
| Thermal Resistance $\theta_{\text {JA, }}$, SOT-23 ${ }^{2}$ | $230^{\circ} \mathrm{C} / \mathrm{W}$ |

[^2]Stresses above those listed under Absolute Maximum Ratings may cause permanent damage to the device. This is a stress rating only; functional operation of the device at these or any other conditions above those indicated in the operational section of this specification is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## ESD CAUTION

|  | ESD (electrostatic discharge) sensitive device. <br> Charged devices and circuit boards can discharge <br> without detection. Although this product features <br> patented or proprietary protection circuitry, damage <br> may occur on devices subjected to high energy ESD. <br> Therefore, proper ESD precautions should be taken to <br> avoid performance degradation or loss of functionality. |
| :--- | :--- |

## PIN CONFIGURATION AND FUNCTION DESCRIPTIONS



Table 3. Pin Function Descriptions

| Pin No. | Mnemonic | Description |
| :---: | :---: | :---: |
| 1 | W | Wiper Terminal W. GND $\leq \mathrm{V}_{\mathrm{w}} \leq \mathrm{V}_{\mathrm{DD}}$. |
| 2 | $V_{D D}$ | Positive Power Supply. Specified for nonOTP operation from 2.7 V to 5.5 V . For OTP programming, $\mathrm{V}_{\text {DD_otp }}$ must be within the window of 4.75 V and 5.25 V and be capable of driving 100 mA . |
| 3 | GND | Common Ground. |
| 4 | SCL | Serial Clock Input. Requires a pull-up resistor. If it is driven directly from a logic controller without the pull-up resistor, ensure that the $\mathrm{V}_{\mathrm{IH}}$ minimum is $0.7 \times \mathrm{V}_{\mathrm{DD}}$. |
| 5 | SDA | Serial Data Input/Output. Requires a pull-up resistor. If it is driven directly from a logic controller without the pull-up resistor, ensure that the $\mathrm{V}_{\mathrm{H}}$ minimum is $0.7 \times \mathrm{V}_{\mathrm{DD}}$. |
| 6 | ADO | $1^{2} \mathrm{C}$ Device Address Bit. Allows a maximum of two AD5273 devices to be addressed. |
| 7 | B | Resistor Terminal B. GND $\leq \mathrm{V}_{\mathrm{B}} \leq \mathrm{V}_{\mathrm{DD}}$. |
| 8 | A | Resistor Terminal A. GND $\leq \mathrm{V}_{\mathrm{A}} \leq \mathrm{V}_{\mathrm{DD}}$. |

## TYPICAL PERFORMANCE CHARACTERISTICS



Figure 3. RINL vs. Code vs. Supply Voltages


Figure 4. R RNL vs. Code vs. Supply Voltages


Figure 5. INL vs. Code vs. Temperature


Figure 6. DNL vs. Code vs. Temperature


Figure 7. INL vs. Code vs. Supply Voltages


Figure 8. DNL vs. Code vs. Supply Voltages


Figure 9. INL vs. Supply Voltage


Figure 10. Rinl vs. Supply Voltage


Figure 11. Full-Scale Error


Figure 12. Zero-Scale Error


Figure 13. Supply Current vs. Temperature


Figure 14. Supply Current vs. Digital Input Voltage

## AD5273



Figure 15. Rheostat Mode Tempco $\left(\Delta R_{w B} / R_{w B}\right) / \Delta T$ vs. Code


Figure 16. Potentiometer Mode Tempco $\left(\Delta V_{w} / V_{w}\right) / \Delta T$ vs. Code


Figure 17. Gain vs. Frequency vs. Code, $R_{A B}=1 \mathrm{k} \Omega$


Figure 18. Gain vs. Frequency vs. Code, $R_{A B}=10 \mathrm{k} \Omega$


Figure 19. Gain vs. Frequency vs. Code, $R_{A B}=50 \mathrm{k} \Omega$


Figure 20. Gain vs. Frequency vs. Code, $R_{A B}=100 \mathrm{k} \Omega$


Figure 21. $-3 d B$ Bandwidth


Figure 22. PSRR vs. Frequency


Figure 23. Digital Feedthrough


Figure 24. Large Settling Time


Figure 25. Midscale Glitch Energy


Figure 26. Power-Up Settling Time After Fuses Blown


Figure 27. Iwb_max vs. Code


Figure 28. OTP Program Energy Plot for Single Fuse


Figure 29. Interface Timing Diagram

## THEORY OF OPERATION

The AD5273 is a one-time programmable (OTP), set-and-forget, 6-bit digital potentiometer. The AD5273 allows unlimited 6-bit adjustments prior to the OTP. OTP technology is a proven costeffective alternative over EEMEM in one-time memory programming applications. The AD5273 employs fuse link technology to achieve the memory retention of the resistance setting function. It comprises six data fuses, which control the address decoder for programming the RDAC, one user mode test fuse for checking setup error, and one programming lock fuse for disabling any further programming once the data fuses are programmed correctly.

## ONE-TIME PROGRAMMING

Prior to OTP activation, the AD5273 presets to midscale during power-on. After the wiper is set to the desired position, the resistance can be permanently set by programming the T bit and the one-time $\mathrm{V}_{\text {DD_otp }}$ to high and by coding the part properly (see Figure 31). The fuse link technology of the

AD5273 requires a Vdd_otp between 4.75 V and 5.25 V to blow the fuses to achieve a given nonvolatile setting. During operation, however, $\mathrm{V}_{\mathrm{DD}}$ can be 2.7 V to 5.5 V . Therefore, a system supply that is lower than 4.75 V requires an external supply for OTP. The user is allowed only one attempt to blow the fuses. If the user fails to blow the fuses on the first attempt, the fuse structure may change such that they can never be blown, regardless of the energy applied during subsequent events. For details, see the Power Supply Considerations section.

The device control circuit has two validation bits, E1 and E0, that can be read back in the read mode to check the programming status, as shown in Figure 32. Users should always read back the validation bits to ensure that the fuses are properly blown. After the fuses have been blown, all fuse latches are enabled upon subsequent power-on; therefore, the output corresponds to the stored setting. Figure 30 shows a detailed functional block diagram.


Figure 30. Detailed Functional Block Diagram


Figure 31. SDA Write Mode Bit Format


Figure 32. SDA Read Mode Bit Format

## SDA Bit Definitions and Descriptions

$\mathrm{S}=$ start condition.
$\mathrm{P}=$ stop condition.
A = acknowledge.
$\mathrm{X}=$ don't care.
$\mathrm{T}=\mathrm{OTP}$ programming bit. Logic 1 programs wiper position permanently.
D5, D4, D3, D2, D1, D0 = data bits.
$\mathrm{E} 1, \mathrm{E} 0=\mathrm{OTP}$ validation bits.
$0,0=$ ready to program.
$0,1=$ test fuse not blown successfully. (For factory setup checking purpose only. Users should not see these combinations.)
$1,0=$ fatal error. Do not retry. Discard the unit.
$1,1=$ programmed successfully. No further adjustments possible.
$\mathrm{AD} 0=\mathrm{I}^{2} \mathrm{C}$ device address bit. Allows maximum of two AD5273s to be addressed.

## VARIABLE RESISTANCE AND VOLTAGE FOR RHEOSTAT MODE

If only the W-to-B or W-to-A terminals are used as variable resistors, the unused A or B terminal can be opened or shorted with W. This operation is called rheostat mode (see Figure 33).


Figure 33. Rheostat Mode Configuration
The nominal resistance, $\mathrm{R}_{A B}$, of the RDAC has 64 contact points accessed by the wiper terminal, plus the B terminal contact if $\mathrm{R}_{\text {wB }}$ is considered. The 6-bit data in the RDAC latch is decoded to select one of the 64 settings. Assuming that a $10 \mathrm{k} \Omega$ part is used, the wiper's first connection starts at Terminal B for Data Register $0 \times 00$. This connection yields a minimum of $60 \Omega$ resistance between Terminal W and Terminal B because of the $60 \Omega$ wiper contact resistance. The second connection is the first tap point, which corresponds to $219 \Omega\left(\mathrm{R}_{\mathrm{W}}=1 \times \mathrm{R}_{A B} / 63+\right.$ $\mathrm{R}_{\mathrm{w}}$ ) for Data Register 0x01, and so on. Each LSB data value increase moves the wiper up the resistor ladder until the last tap point is reached at $10,060 \Omega\left(63 \times \mathrm{R}_{A B} / 63+\mathrm{R}_{\mathrm{W}}\right)$. Figure 34 shows a simplified diagram of the equivalent RDAC circuit. The general equation determining $\mathrm{R}_{\text {wв }}$ is

$$
\begin{equation*}
R_{W B}(D)=\frac{D}{63} \times R_{A B}+R_{W} \tag{1}
\end{equation*}
$$

where:
$D$ is the decimal equivalent of the 6-bit binary code.
$R_{A B}$ is the end-to-end resistance.
$R_{W}$ is the wiper resistance contributed by the on resistance of the internal switch.

Table 4. Rwb vs. Codes; $\mathrm{R}_{\mathrm{AB}}=10 \mathrm{k} \Omega$; Terminal A Opened

| D (Dec) | RwB $(\boldsymbol{\Omega})$ | Output State |
| :--- | :--- | :--- |
| 63 | 10,060 | Full scale (RAB $\left.+\mathrm{Rw}_{\mathrm{w}}\right)$ |
| 32 | 5139 | Midscale |
| 1 | 219 | 1 LSB |
| 0 | 60 | Zero scale (wiper contact resistance) |

Because a finite wiper resistance of $60 \Omega$ is present in the zeroscale condition, care should be taken to limit the current flow between W and B in this state to a maximum pulse current of 20 mA . Otherwise, degradation or possible destruction of the internal switch contact can occur.

Similar to the mechanical potentiometer, the resistance of the RDAC between the Wiper W and Terminal A also produces a complementary resistance, $\mathrm{R}_{\mathrm{wA}}$. When these terminals are used, Terminal B can be opened or shorted to W. Setting the resistance value for $\mathrm{R}_{\mathrm{WA}}$ starts at a maximum value of resistance and decreases as the data loaded in the latch increases in value.

The general equation for this operation is

$$
\begin{equation*}
R_{W A}(D)=\frac{63-D}{63} \times R_{A B}+R_{W} \tag{2}
\end{equation*}
$$

Table 5. $\mathrm{R}_{\mathrm{WA}}$ vs. Codes; $\mathrm{R}_{\mathrm{AB}}=10 \mathrm{k} \Omega$; Terminal B Opened

| D (Dec) | Rwa $\boldsymbol{( \Omega )}$ | Output State |
| :--- | :--- | :--- |
| 63 | 60 | Full scale |
| 32 | 4980 | Midscale |
| 1 | 9901 | 1 LSB |
| 0 | 10,060 | Zero scale |

The typical distribution of the resistance tolerance from device to device is process-lot dependent, and it is possible to have $\pm 30 \%$ tolerance.


Figure 34. AD5273 Equivalent RDAC Circuit

## VARIABLE RESISTANCE AND VOLTAGE FOR POTENTIOMETER MODE

If all three terminals are used, the operation is called the potentiometer mode. The most common configuration is the voltage divider operation (see Figure 35).


Figure 35. Potentiometer Mode Configuration
Ignoring the effect of the wiper resistance, the transfer function is simply

$$
\begin{equation*}
V_{W}(D)=\frac{D}{63} V_{A} \tag{3}
\end{equation*}
$$

A more accurate calculation, which includes the wiper resistance effect, yields

$$
\begin{equation*}
V_{W}(D)=\frac{\frac{D}{63} R_{A B}+R_{W}}{R_{A B}+2 R_{W}} V_{A} \tag{4}
\end{equation*}
$$

Unlike rheostat mode where the absolute tolerance is high, potentiometer mode yields an almost ratiometric function of D/63 with a relatively small error contributed by the Rw terms. Therefore, the tolerance effect is almost cancelled. Although the step resistor, $\mathrm{R}_{\mathrm{s}}$, and CMOS switch resistor, $\mathrm{R}_{\mathrm{w}}$, have very different temperature coefficients, the ratiometric adjustment also reduces the overall temperature coefficient effect to $5 \mathrm{ppm} /{ }^{\circ} \mathrm{C}$, except at low value codes where $\mathrm{R}_{\mathrm{w}}$ dominates.
Potentiometer mode includes op amp feedback resistor networks and other voltage scaling applications. Terminal A, Terminal W, and Terminal B can in fact be input or output terminals, provided that $\left|V_{A B}\right|,\left|V_{W A}\right|$, and $\left|V_{W B}\right|$ do not exceed $V_{D D}$ to GND.

## ESD PROTECTION

Digital inputs SDA and SCL are protected with a series input resistor and parallel Zener ESD structures (see Figure 36).


Figure 36. ESD Protection of Digital Pins

## TERMINAL VOLTAGE OPERATING RANGE

There are also ESD protection diodes between $V_{\text {DD }}$ and the RDAC terminals. The $V_{D D}$ of AD5273 therefore defines their voltage boundary conditions (see Figure 37). Supply signals present on Terminal A, Terminal B, and Terminal W that exceed $\mathrm{V}_{\mathrm{DD}}$ are clamped by the internal forward-biased diodes.


Figure 37. Maximum Terminal Voltages Set by $V_{D D}$

## POWER-UP/POWER-DOWN SEQUENCES

Because of the ESD protection diodes, it is important to power $V_{D D}$ first before applying any voltages to Terminal A, Terminal B, and Terminal W. Otherwise, the diode is forward-biased such that $V_{D D}$ is powered unintentionally and can affect the rest of the user's circuits. The ideal power-up sequence is in the following order: GND, $V_{D D}$, digital inputs, and $V_{A} / V_{B} / V_{W}$. The order of powering $\mathrm{V}_{\mathrm{A}}, \mathrm{V}_{\mathrm{B}}, \mathrm{V}_{\mathrm{W}}$, and digital inputs is not important as long as they are powered after $V_{\text {DD }}$. Similarly, $\mathrm{V}_{\mathrm{DD}}$ should be powered down last.

## POWER SUPPLY CONSIDERATIONS

To minimize the package pin count, both OTP and normal operating voltage supplies are applied to the same $V_{D D}$ terminal of the AD5273. The AD5273 employs fuse link technology that requires 4.75 V to 5.25 V for blowing the internal fuses to achieve a given setting, but normal $V_{D D}$ can be in the range of 2.7 V to
5.5 V after completing the fuse programming process. As a result, dual voltage supplies and isolation are needed if the system $V_{D D}$ is outside the required $V_{\text {DD_отP }}$ range. For successful OTP, the fuse programming supply (either an on-board regulator or rack-mount power supply) must be rated at 4.75 V to 5.25 V and provide a 100 mA current for 400 ms . Once fuse programming is completed, the $\mathrm{V}_{\mathrm{DD} \_ \text {otp }}$ supply must be removed to allow normal operation of 2.7 V to 5.5 V ; then the device reduces the current consumption to the $\mu \mathrm{A}$ range.
When operating systems at 2.7 V , use of the bidirectional low threshold P-Ch MOSFETs is recommended for the supply's isolation. As shown in Figure 38, this assumes that the 2.7 V system voltage is applied first and that the P1 and P2 gates are pulled to ground, thus turning on P1 first and then P2. As a result, $V_{\text {DD }}$ of the AD5273 approaches 2.7 V . When the AD5273 setting is found, the factory tester applies the $V_{\text {DD_otp }}$ to both the VDD and the MOSFETs' gates, thus turning off P1 and P2. The OTP command should be executed at this time to program the AD5273 while the 2.7 V source is protected. Once the fuse programming is complete, the tester withdraws the $\mathrm{V}_{\text {DD_отP }}$ and the AD5273's setting is fixed permanently.


Figure 38. 5 V OTP Supply Isolated from the 2.7 V Normal Operating Supply
AD5273 achieves the OTP function through blowing internal fuses. Users should always apply the 4.75 V to 5.25 V OTP voltage requirement at the first fuse programming attempt. Failure to comply with this requirement can lead to a change in fuse structures, rendering programming inoperable.
Care should be taken when SCL and SDA are driven from a low voltage logic controller. Users must ensure that the logic high level is between $0.7 \times V_{\mathrm{DD}}$ and $\mathrm{V}_{\mathrm{DD}}$. Refer to the Level Shift for Different Voltages Operation section.
Poor PCB layout introduces parasitics that can affect fuse programming. Therefore, it is recommended to add a $10 \mu \mathrm{~F}$ tantalum capacitor in parallel with a 1 nF ceramic capacitor as close as possible to the $V_{D D}$ pin. The type and value chosen for both capacitors are important. This combination of capacitor values provides a fast response and larger supply current handling with minimum supply drop during transients. As a result, these capacitors increase the OTP programming success by not inhibiting the proper energy needed to blow the internal fuses. Additionally, C 1 minimizes transient disturbance and low frequency ripple, while C 2 reduces high frequency noise during normal operation.

## CONTROLLING THE AD5273

To control the AD5273, users can program the device with either computer software or with external $\mathrm{I}^{2} \mathrm{C}$ controllers.

## SOFTWARE PROGRAMMING

Because of the OTP feature, users can program the AD5273 in the factory before shipping it to end users. Therefore, Analog Devices offers device programming software that can be implemented in the factory on computers running Windows NT, Windows 2000, and Windows XP platforms. The software, which can be downloaded from the AD5273 product page at www.analog.com, is an executable file that does not require any programming languages or user programming skills. Figure 39 shows the software interface.


Figure 39. Software Interface

## Write

The AD5273 starts at midscale after power-up prior to any OTP programming. To increment or decrement the resistance, move the scrollbar on the left. Once the desired setting is found, click Program Permanent to lock the setting permanently. To write any specific values, use the bit pattern control in the upper section and click Run. The format of writing data to the device is shown in Figure 31. Once the desired setting is found, set the T bit to 1 and click Run to program the setting permanently.

## Read

To read the validation bits and data from the device, click Read. The user can also set the bit pattern in the upper section and click Run. The format of reading data from the device is shown in Figure 32.

To control the device in both read and write operations, the program generates the $\mathrm{I}^{2} \mathrm{C}$ digital signals through the parallel port LPT1 Pin 2, Pin 3, Pin 15, and Pin 25 for SDA_write, SCL, SDA_read, and DGND, respectively (see Figure 40).
To apply the device programming software in the factory, lay out the AD5273 SCL and SDA pads on the PCB such that the programming signals can be communicated to and from the parallel port (see Figure 40). Figure 41 shows a recommended AD5273 PCB layout into which pogo pins can be inserted for factory programming. To prevent damaging the PC parallel port, $100 \Omega$ resistors should also be put in series to the SCL and SDA pins. Pull-up resistors on SCL and SDA are also required.


Figure 40. Parallel Port Connection; Pin $2=$ SDA_Write, Pin $3=S C L$, Pin $15=$ SDA_Read, and Pin $25=$ DGND


Figure 41. Recommended AD5273 PCB Layout

## $I^{2}$ C CONTROLLER PROGRAMMING

## Write Bit Patterns



Figure 42. Writing to the RDAC Register


## Read Bit Pattern



Figure 44. Reading Data from the RDAC Register

For users who do not use the software solution, the AD5273 can be controlled via an $\mathrm{I}^{2} \mathrm{C}$-compatible serial bus and is connected to this bus as a slave device. Referring to Figure 42, Figure 43, and Figure 44, the 2 -wire $\mathrm{I}^{2} \mathrm{C}$ serial bus protocol operates as follows:

1. The master initiates data transfer by establishing a start condition. A start condition is defined as a high-to-low transition on the SDA line while SCL is high, as shown in Figure 42 . The byte following the start condition is the slave address byte, which consists of six MSBs defined as 010110. The next bit is AD 0 ; it is an $\mathrm{I}^{2} \mathrm{C}$ device address bit. Depending on the states of the AD0 bits, two AD5273s can be addressed on the same bus, as shown in Figure 45. The last LSB is the $\mathrm{R} / \overline{\mathrm{W}}$ bit, which determines whether data is read from or written to the slave device.

The slave address corresponding to the transmitted address responds by pulling the SDA line low during the ninth clock pulse (this is termed the acknowledge bit). At this stage, all other devices on the bus remain idle while the selected device waits for data to be written to or read from its serial register.
2. A write operation contains one more instruction byte than the read operation. The instruction byte in the write mode follows the slave address byte. The MSB of the instruction byte labeled T is the OTP bit. After acknowledging the instruction byte, the last byte in the write mode is the data byte. Data is transmitted over the serial bus in sequences of nine clock pulses (eight data bits followed by an acknowledge bit). The transitions on the SDA line must occur during the low period of SCL and remain stable during the high period of SCL, as shown in Figure 42.
3. In read mode, the data byte follows immediately after the acknowledgment of the slave address byte. Data is transmitted over the serial bus in sequences of nine clock pulses (slight difference from write mode, there are eight data bits followed by a no acknowledge bit). Similarly, the transitions on the SDA line must occur during the low period of SCL and remain stable during the high period of SCL, as shown in Figure 44.
4. When all data bits have been read or written, a stop condition is established by the master. A stop condition is defined as a low-to-high transition on the SDA line while SCL is high. In write mode, the master pulls the SDA line high during the $10^{\text {th }}$ clock pulse to establish a stop condition, as shown in Figure 42 and Figure 43. In read mode, the master issues a no acknowledge for the ninth clock pulse, that is, the SDA line remains high. The master then brings the SDA line low before the $10^{\text {th }}$ clock pulse, which goes high to establish a stop condition, as shown in Figure 44.

A repeated write function gives the user flexibility to update the RDAC output continuously, except after permanent programming, when the part is addressed and receives instructions only once. During the write cycle, each data byte updates the RDAC output. For example, after the RDAC has acknowledged its slave address and instruction bytes, the RDAC output updates after these two bytes. If another byte is written to the RDAC while it is still addressed to a specific slave device with the same instruction, this byte updates the output of the selected slave device. If different instructions are needed, the write mode must be started again with a new slave address, instruction, and data bytes. Similarly, a repeated read function of the RDAC is also allowed.

## CONTROLLING TWO DEVICES ON ONE BUS

Figure 45 shows two AD5273 devices on the same serial bus. Each has a different slave address because the state of each AD0 pin is different. This allows each device to operate independently. The master device output bus line drivers are open-drain pulldown in a fully $\mathrm{I}^{2} \mathrm{C}$-compatible interface.


Figure 45. Two AD5273 Devices on One Bus

## APPLICATIONS INFORMATION

## DAC

It is common to buffer the output of the digital potentiometer as a DAC. The buffer minimizes the load dependence and delivers higher current to the load, if needed.


Figure 46. Programmable Voltage Reference (DAC)

## PROGRAMMABLE VOLTAGE SOURCE WITH BOOSTED OUTPUT

For applications that require high current adjustment, such as a laser diode driver or tunable laser, consider a booster voltage source, as shown in Figure 47.


Figure 47. Programmable Booster Voltage Source
In this circuit, the inverting input of the op amp forces the Vour to be equal to the wiper voltage set by the digital potentiometer. The load current is then delivered by the supply via the N -Channel FET, $\mathrm{N}_{1} . \mathrm{N}_{1}$ power handling must be adequate to dissipate $\left(\mathrm{V}_{\text {IN }}-\mathrm{V}_{\text {OUT }}\right) \times \mathrm{I}_{\mathrm{L}}$ power. This circuit can source a maximum of 100 mA with a 5 V supply. For precision applications, a voltage reference, such as the ADR421, ADR03, or ADR370, can be applied at Terminal A of the digital potentiometer.

## PROGRAMMABLE CURRENT SOURCE

A programmable current source can be implemented with the circuit shown in Figure 48. The load current is the voltage across Terminal B to Terminal W of the AD5273 divided by Rs. At zero scale, Terminal A of the AD5273 is -2.048 V , which makes the wiper voltage clamped at ground potential. Depending on the load, Equation 5 is therefore valid only at certain codes. For example, when the compliance voltage, $\mathrm{V}_{\mathrm{L}}$, equals half of $\mathrm{V}_{\text {REF }}$, the current can be programmed from midscale to full scale of the AD5273.


Figure 48. Programmable Current Source

$$
\begin{equation*}
\left.I_{L}=\frac{\left(V_{R E F} \times D\right) / 64}{R_{S}} \right\rvert\, 32 \leq D \leq 63 \tag{5}
\end{equation*}
$$

## GAIN CONTROL COMPENSATION

As shown in Figure 49, the digital potentiometers are commonly used in gain controls or sensor transimpedance amplifier signal conditioning applications.


Figure 49. Typical Noninverting Gain Amplifier
In both applications, one of the digital potentiometer terminals is connected to the op amp inverting node with finite terminal capacitance, C1. It introduces a zero for the $1 \beta_{o}$ term with $20 \mathrm{~dB} / \mathrm{dec}$, whereas a typical op amp GBP has $-20 \mathrm{~dB} / \mathrm{dec}$ characteristics. A large R 2 and finite C 1 can cause this zero's frequency to fall well below the crossover frequency. Therefore, the rate of closure becomes $40 \mathrm{~dB} / \mathrm{dec}$ and the system has a $0^{\circ}$ phase margin at the crossover frequency. The output may ring, or in the worst case, oscillate when the input is a step function. Similarly, it is also likely to ring when switching between two gain values because this is equivalent to a step change at the input. To reduce the effect of C 1 , users should also configure Terminal B or Terminal A rather than Terminal W at the inverting node.

## AD5273

Depending on the op amp GBP, reducing the feedback resistor may extend the zero's frequency far enough to overcome the problem. A better approach is to include a compensation capacitor, C 2 , to cancel the effect caused by C1. Optimum compensation occurs when $\mathrm{R} 1 \times \mathrm{C} 1=\mathrm{R} 2 \times \mathrm{C} 2$, but this is not an option because of the variation of R2. As a result, users can use the relationship described and scale C2 as if R2 were at its maximum value. However, doing so may overcompensate by slowing down the settling time when R2 is set to low values. To avoid this problem, C 2 should be found empirically for a given application. In general, setting C2 in the range of a few picofarads to no more than a few tenths of a picofarad is usually adequate for compensation.
There is also a Terminal W capacitance connected to the output (not shown); its effect on stability is less significant; therefore, compensation is not necessary unless the op amp is driving a large capacitive load.

## PROGRAMMABLE LOW-PASS FILTER

In ADC applications, it is common to include an antialiasing filter to band-limit the sampling signal. To minimize various system redesigns, users can use two $1 \mathrm{k} \Omega$ AD5273s to construct a generic second-order Sallen-Key low-pass filter. Because the AD5273 is a single-supply device, the input must be dc offset when an ac signal is applied to avoid clipping at ground. This is illustrated in Figure 50. The design equations are

$$
\begin{align*}
& \frac{V_{O}}{V_{I}}=\frac{\omega_{0}{ }^{2}}{S^{2}+\frac{\omega_{O}}{Q} S+\omega_{O}^{2}}  \tag{6}\\
& \omega_{O}=\sqrt{\frac{1}{\text { RIR2C1C2 }}}  \tag{7}\\
& Q=\frac{1}{\text { R1C1 }}+\frac{1}{\text { R2C2 }} \tag{8}
\end{align*}
$$

Users can first select some convenient values for the capacitors. To achieve maximally flat bandwidth where $\mathrm{Q}=0.707$, let C 1 be twice the size of C2 and let R1 = R2. As a result, R1 and R2 can be adjusted to the same setting to achieve the desired bandwidth.


Figure 50. Sallen Key Low-Pass Filter

## LEVEL SHIFT FOR DIFFERENT VOLTAGES OPERATION

If the SCL and SDA signals come from a low voltage logic controller and are below the minimum $\mathrm{V}_{\mathrm{IH}}$ level $\left(0.7 \times \mathrm{V}_{\mathrm{DD}}\right)$, level-shift the signals for successful read/write communication between the AD5273 and the controller. Figure 51 shows one of the implementations. For example, when SDA1 is 2.5 V , M1 turns off, and SDA2 becomes 5 V . When SDA1 is 0 V , M1 turns on, and SDA2 approaches 0 V . As a result, proper level-shifting is established. M1 and M2 should be low threshold N -Channel power MOSFETs, such as FDV301N.


Figure 51. Level Shift for Different Voltages Operation

## RDAC CIRCUIT SIMULATION MODEL

The internal parasitic capacitances and the external capacitive loads dominate the ac characteristics of the digital potentiometers. Configured as a potentiometer divider, the -3 dB bandwidth of the AD5273 ( $1 \mathrm{k} \Omega$ resistor) measures 6 MHz at half scale. Figure 17 to Figure 20 provide the large signal BODE plot characteristics of the four available resistor versions: $1 \mathrm{k} \Omega$, $10 \mathrm{k} \Omega, 50 \mathrm{k} \Omega$, and $100 \mathrm{k} \Omega$. Figure 52 shows a parasitic simulation model. The code following Figure 52 provides a macro model net list for the $1 \mathrm{k} \Omega$ device.


Figure 52. Circuit Simulation Model for RDAC $=1 \mathrm{k} \Omega$

```
Macro Model Net List for RDAC
.PARAM D = 63, RDAC = 1E3
*
.SUBCKT DPOT (A,W,B)
*
CA A 0 25E-12
RWA A W {(1-D/63)*RDAC+60}
CW W 0 55E-12
RWB W B {D/63*RDAC+60}
CB B 0 25E-12
*
.ENDS DPOT
```


## EVALUATION BOARD



Figure 53. Evaluation Board Schematic


Figure 54. One Possible Configuration-
Programmable Voltage Reference

## OUTLINE DIMENSIONS



Figure 56. 8-Lead Small Outline Transistor Package [SOT-23]
(RJ-8)
Dimensions shown in millimeters

| Model | $\mathrm{R}_{\text {AB }}(\mathrm{k} \Omega)$ | Temperature Range | Package Option | Package Description | Ordering Quantity | Branding |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AD5273BRJ1-R2 | 1 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 | 250 | DYA |
| AD5273BRJ1-REEL7 | 1 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 | 3,000 | DYA |
| AD5273BRJZ1-REEL7 ${ }^{1}$ | 1 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 | 3,000 | DYE |
| AD5273BRJ10-R2 | 10 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 | 250 | DYB |
| AD5273BRJ10-REEL7 | 10 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 | 3,000 | DYB |
| AD5273BRJZ10-REEL71 | 10 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 | 3,000 | DYF |
| AD5273BRJ50-R2 | 50 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 | 250 | DYC |
| AD5273BRJ50-REEL7 | 50 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 | 3,000 | DYC |
| AD5273BRJZ50-REEL71 | 50 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 | 3,000 | DYG |
| AD5273BRJ100-R2 | 100 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 | 250 | DYD |
| AD5273BRJ100-REEL7 | 100 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 | 3,000 | DYD |
| AD5273BRJZ100-REEL7 ${ }^{1}$ AD5273EVAL ${ }^{2}$ | 100 | $-40^{\circ} \mathrm{C}$ to $+105^{\circ} \mathrm{C}$ | RJ-8 | 8-Lead SOT-23 <br> Evaluation Board | 3,000 | DYH |

[^3]NOTES

## NOTES

Purchase of licensed $I^{2} C$ components of Analog Devices or one of its sublicensed Associated Companies conveys a license for the purchaser under the Philips $I^{2} C$ Patent Rights to use these components in an $I^{2} C$ system, provided that the system conforms to the $I^{2} C$ Standard Specification as defined by Philips.


[^0]:    ${ }^{1}$ OTP allows unlimited adjustments before permanent setting.
    ${ }^{2}$ Analog Devices cannot guarantee the software to be $100 \%$ compatible to all systems due to the wide variation in computer configurations.
    ${ }^{3}$ Applies to $1 \mathrm{k} \Omega$ parts only.
    ${ }^{4}$ The terms digital potentiometer, VR, and RDAC are used interchangeably.

[^1]:    ${ }^{1}$ Typical values represent average readings at $25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V}$, and $\mathrm{V}_{S S}=0 \mathrm{~V}$.
    ${ }^{2}$ Resistor position nonlinearity error, $\mathrm{R}-\mathrm{INL}$, is the deviation from an ideal value measured between the maximum resistance and the minimum resistance wiper positions. R-DNL measures the relative step change from ideal between successive tap positions. Parts are guaranteed monotonic.
    ${ }^{3} V_{A B}=V_{D D}$, wiper $\left(V_{w}\right)=$ no connect.
    ${ }^{4} \Delta R_{w B} / \Delta T=\Delta R_{w A} / \Delta T$. Temperature coefficient is code-dependent; see the Typical Performance Characteristics section.
    ${ }^{5}$ INL and DNL are measured at $\mathrm{V}_{\mathrm{w}}$. INL with the RDAC configured as a potentiometer divider similar to a voltage output DAC. V $\mathrm{V}_{\mathrm{w}}$ with the RDAC configured as a potentiometer divider similar to a voltage output $\mathrm{DAC} . \mathrm{V}_{\mathrm{A}}=\mathrm{V}_{\mathrm{DD}}$ and $\mathrm{V}_{\mathrm{B}}=0 \mathrm{~V}$. DNL specification limits of $\pm 1$ LSB maximum are guaranteed monotonic operating conditions.
    ${ }^{6}$ The A, B, and W resistor terminals have no limitations on polarity with respect to each other.
    ${ }^{7}$ Guaranteed by design; not subject to production test.
    ${ }^{8}$ The minimum voltage requirement on the $\mathrm{V}_{H}$ is $0.7 \times \mathrm{V}_{\mathrm{DD}}$. For example, $\mathrm{V}_{H H} \min =3.5 \mathrm{~V}$ when $\mathrm{V}_{D D}=5 \mathrm{~V}$. It is typical for the SCL and SDA resistors to be pulled up to $\mathrm{V}_{\mathrm{DD}}$. However, care must be taken to ensure that the minimum $\mathrm{V}_{\mathbb{H}}$ is met when the SCL and SDA are driven directly from a low voltage logic controller without pull-up resistors.
    ${ }^{9}$ Different from the operating power supply; the power supply for OTP is used one time only.
    ${ }^{10}$ Different from the operating current; the supply current for OTP lasts approximately 400 ms for the one time it is needed.
    ${ }^{11}$ See Figure 28 for the energy plot during the OTP program.
    ${ }^{12} \mathrm{P}_{\text {DISS }}$ is calculated from ( $\mathrm{I}_{\mathrm{DD}} \times \mathrm{V}_{\mathrm{DD}}$ ). CMOS logic level inputs result in minimum power dissipation.
    ${ }^{13}$ Bandwidth, noise, and settling time depend on the terminal resistance value chosen. The lowest $R$ value results in the fastest settling time and highest bandwidth.
    The highest R value results in the minimum overall power consumption.
    ${ }^{14}$ All dynamic characteristics use $\mathrm{V}_{\mathrm{DD}}=5 \mathrm{~V}$.
    ${ }^{15}$ See Figure 29 for the location of the measured values.

[^2]:    ${ }^{1}$ Maximum terminal current is bounded by the maximum current handling of the switches, the maximum power dissipation of the package; the maximum applied voltage across any two of the A, B, and W terminals at a given resistance.
    ${ }^{2}$ Package power dissipation $=\left(T_{\jmath} \max -T_{A}\right) / \theta_{J A}$.

[^3]:    ${ }^{1} Z=$ RoHS Compliant Part.
    ${ }^{2}$ Users should order samples because the evaluation kit comes with a socket, but does not include the parts.

